## Eddy Current Losses in Active Clamp Forward Converter

To check the Eddy Current Losses influence on the Active Clamp Forward Converter efficiency the two transformer on the same breadboard were replaced. One transformer had the secondary winding made by some thin wires to get eddy current losses as minimum. The secondary winding of the second transformer was made by one wire with the same DC resistance as the first one. The same core and coil former with both primary and bias windings was used, the secondary winding was replaced only.

## Converter Parameters:

Vin $=299 \mathrm{VDC}$
Vout $=5 \mathrm{VDC}$
Iout $=15 \mathrm{~A}$
$\mathrm{F}_{\text {SW }}=119 \mathrm{kHz}$
$\mathrm{D}=0.37$
$\Delta \mathrm{I}_{\mathrm{SEC}}=4.5 \mathrm{AP}-\mathrm{P}$

## Transformer specification:

Core: ETD-29
Ferrite: N87 by Epcos
Air gap: appr. 0.2 mm to meet the primary inductance 3.2 mH
Primary: 86T $\quad 0.19 \mathrm{~mm}$
Bias: $2 \mathrm{~T} \quad \varnothing 0.1 \mathrm{~mm}$
Secondary - Var. 1:
4T 16 stranded wires $\emptyset 0.41 \mathrm{~mm}$
$\mathrm{R}_{\mathrm{DC}}=1.82 \mathrm{~m} \Omega$
$\mathrm{R}_{\mathrm{AC}} / \mathrm{R}_{\mathrm{DC}}=1.3$ for one layer
$\mathrm{R}_{\mathrm{AC}}=2.37 \mathrm{~m} \Omega$
Secondary - Var. 2:
$4 \mathrm{~T} \quad \varnothing 1.7 \mathrm{~mm}$.
$\mathrm{R}_{\mathrm{DC}}=1.83 \mathrm{~m} \Omega$
$\mathrm{R}_{\mathrm{AC}} / \mathrm{R}_{\mathrm{DC}}=4.5$ for one layer
$\mathrm{R}_{\mathrm{AC}}=8.24 \mathrm{~m} \Omega$

RMS of secondary current is the same for both variants:
$\mathrm{I}_{\mathrm{DC}}=\mathrm{I}_{\mathrm{OUT}} * \mathrm{D}=16 \mathrm{~A} * 0.37=5.92 \mathrm{~A}$
$\mathrm{I}_{\mathrm{AC}}=\mathrm{I}_{\mathrm{OUT}} * \sqrt{(\mathrm{D} *(1-\mathrm{D})}=16 \mathrm{~A} * \sqrt{0.37 *(1-0.37)}=7.72 \mathrm{~A}$
So we must get the secondary winding losses:
Var. 1:
$\mathrm{P}_{\mathrm{\Sigma} 1}=\mathrm{R}_{\mathrm{DC}} * \mathrm{I}_{\mathrm{DC}}^{2}+\mathrm{R}_{\mathrm{AC}} * \mathrm{I}_{\mathrm{AC}}^{2}=1.82 \mathrm{~m} \Omega * 5.92 \mathrm{~A}^{2}+2.37 \mathrm{~m} \Omega * 7.72 \mathrm{~A}^{2}=205 \mathrm{~mW}$
Var. 2:
$\mathrm{P}_{\Sigma 2}=\mathrm{R}_{\mathrm{DC}} * \mathrm{I}_{\mathrm{DC}}^{2}+\mathrm{R}_{\mathrm{AC}} * \mathrm{I}_{\mathrm{AC}}^{2}=1.83 \mathrm{~m} \Omega * 5.92 \mathrm{~A}^{2}+8.24 \mathrm{~m} \Omega * 7.72 \mathrm{~A}^{2}=555 \mathrm{~mW}$
This difference $\mathrm{P}_{\Sigma^{1}}-\mathrm{P}_{\Sigma^{2}}=350 \mathrm{~mW}$ should be see in the input current as:

$$
\Delta \mathrm{I}_{\mathrm{IN}}=\frac{\mathrm{P}_{\Sigma 1}-\mathrm{P}_{\Sigma 2}}{\mathrm{~V}_{\mathrm{IN}}}=\frac{350 \mathrm{~mW}}{299 \mathrm{~V}}=1.17 \mathrm{~mA}
$$

## Test set-up and conditions:

Input voltage, Input Current, Output Voltage and Output Current were measured by ESCORT model 95T Multimeters.

The input voltage was provided by B5-50 299VDC, 299 mA power supply.
The output was loaded by KIKUSUI model PLZ303W electronic load.
Primary current and drain voltage were monitored by Tektronix model TDS210 oscilloscope.
The full load (15A) was applied for appr. 20min to get stabile temperature on all components. Test was performed at $25^{\circ} \mathrm{C}$ with no airflow.

## Test results:

## Variant 1:

$$
\begin{aligned}
& \mathrm{V}_{\text {IV }}=299.37 \mathrm{~V} \\
& \mathrm{I}_{\text {IN }}=280.50 \mathrm{~mA} \\
& \mathrm{~V}_{\text {OUT }}=5.023 \mathrm{~V} \\
& \mathrm{I}_{\text {OUT }}=15.005 \mathrm{~A} \\
& \text { Eff. }=89.75 \%
\end{aligned}
$$

## Variant 2:

$\mathrm{V}_{\text {IN }}=299.51 \mathrm{~V}$
$\mathrm{I}_{\mathrm{IN}}=280.37 \mathrm{~mA}$
$\mathrm{V}_{\text {OUt }}=5.023 \mathrm{~V}$
$\mathrm{I}_{\text {Out }}=15.005 \mathrm{~A}$
Eff. $=89.75 \%$

The drain voltage waveforms:


The Primary Current waveforms:


The Schematic diagram and Bill of Materials are shown below:


| Qty | Ref. Des. | Part Number | Manufacturer | Description |
| :---: | :---: | :---: | :---: | :---: |
| 2 | C1, C2 | B81122-C1102 | Epcos | EMI Supression Capacitor, Y2 |
| 1 | C14 | GRM2165C2A101JA01D | Murata | 100pF, 100V, NP0, 0603 Ceramic |
| 3 | C15, C16, C21 | No Load |  |  |
| 1 | C17 | DE1B3KX472M | Murata | Class Y1 Cap., 4700pF |
| 2 | C18, 19 | EXR471M25B | Hitano | 470uF, 25V, Low ESR, 10*16 Al. Cap. |
| 1 | C20 | ECJ-4YB0J226M | Panasonic-ECG | 22uF, 6V, X5R, 1210 Ceramic |
| 1 | C3 | B81131-D1104 | Epcos | X2 MKT Cap. 0.1uF |
|  | C4 | KMH401E101MP30S | Nippon Chemi-Con | $100 \mathrm{FF}, 400 \mathrm{~V}, 25 * 25 \mathrm{Al}$. Cap. |
| 1 | C5 | ECJ-1VB1H103K | Panasonic-ECG | $0.01 \mathrm{uF}, 500 \mathrm{~V}, \mathrm{X7R}, 1206$ Ceramic |
| 4 | $\begin{aligned} & \mathrm{C} 6, \mathrm{C} 12, \mathrm{C} 13, \\ & \mathrm{C} 22 \end{aligned}$ | ECJ-1VB1E104K | Panasonic-ECG | 0.1uF, 25V, X7R, 0603 Ceramic |
| 4 | $\begin{aligned} & \text { C7, C8, C10, } \\ & \text { C11 } \end{aligned}$ | ECJ-1VB1C105K | Panasonic-ECG | 1uF, 16V, X5R, 0603 Ceramic |
| 1 | C9 | EHR470M50B | Hitano | $47 \mathrm{uF}, 50 \mathrm{~V}, 6.3 \times 11,-40 . .+105^{\circ} \mathrm{C} \mathrm{Al}$. |
| 1 | D1 | RS-205 | DC components | 2A, 600V SIP Bridge Rectifier |
| 1 | D2 | BAV99 | Philips | Series, General Purpose |
| 5 | $\begin{aligned} & \text { D3, D5, } \\ & \text { D6 - D8 } \end{aligned}$ | No Load |  |  |
| 1 | D4 | BAS16 | Philips | General, 75V, 200mA, SOT-23 |
| 1 | D9 | FYL-30004ET | Foryard | LED Red 3mm through-hole |
| 1 | F1 | FH-101 |  | 5*20 TroughHole Fuse Holder |
|  | J1 | DG305-02V2 | Degson | 10mm Terminal Block, 2 term. |
| 1 | J3 | DG25C-04 | Degson | 300mil Terminal Block, 4 term. |
| 1 | L1 |  |  | AC Common mode choke |
| 1 | L2 |  |  | 8.7uH, Core T90-26 Ring, 11T 7*0.8 Inductor |
| 1 | L3 | SC5020-R50M | EMC | 0.5", 24A SMT Power Inductor |
| 1 | Q1 | IRFBC40 | IR | $600 \mathrm{~V}, 1.2$ Ohm, N-Channel MOSFET, TO-220 |
| 1 | Q2 | IRFRC20 | IR | N-ch MOSFET, 600 V ,2A, 4.4Ohm, DPAK |
| 3 | Q3, Q6, Q7 | No Load |  |  |
| 2 | Q4, Q5 | IRLR7833 | IR | N-ch MOSFET, 600V ,2A, 4.4Ohm, DPAK |
| 1 | R1 | SCK-472 | Voltts | NTC termistor 47Ohm 2A |
| 1 | R10 | CR0603JW114 | Bourns | 110kOhm, 0603, 5\% resistor |
| 1 | R11 | CR0603FW3301 | Bourns | 3.3kOhm, 0603, 1\% resistor |
| 3 | R12, R25, R27 | CR0603000 | Bourns | 0 Ohm, 0603 resistor |
| 6 | R13, R14, R31, R33, R21, R26, R28 | No Load |  | 1 KOhm, 0603, 5\% resistor |
| 1 | R15 | CR0603FW2001 | Bourns | 2kOhm, 0603, 1\% resistor |
| 1 | R16 | CR0603FW2202 | Bourns | 22kOhm, 0603, 1\% resistor |
| 1 | R17 | CR0603FW1503 | Bourns | 150kOhm, 0603, 1\% resistor |
| 1 | R18 | CR0603FW1803 | Bourns | 180kOhm, 0603, 1\% resistor |
| 1 | R19 | CR0603FW5602 | Bourns | 56kOhm, 0603, 1\% resistor |
| 1 | R2 | CR1206JW1R0 | Bourns | 1 Ohm, 1206, 5\% resistor |
| 3 | R22-R24 | CR1206JW1R5 | Bourns | 1.5 Ohm, 1206, $5 \%$ resistor |
| 4 | $\begin{aligned} & \text { R7, R20, R29, } \\ & \text { R30 } \end{aligned}$ | CR0603JW102 | Bourns | 1K, 0603, 5\% resistor |
| 3 | R32, R34, R35 | CR0603FW1002 | Bourns | 10K, 0603, 1\% resistor |
| 2 | R3, R4 | CR1206JW153 | Bourns | 150kOhm, 1206, $5 \%$ resistor |
| 2 | R5, R6 | CR1206FW4702 | Bourns | Resistor 5\% Any Value 1206 |
| 1 | R8 | CR0603JW913 | Bourns | 91K, 0603, $5 \%$ resistor |
| 1 | R9 | CR0603FW3601 | Bourns | 3.6K, 0603, 1\% resistor |
|  | T1 |  |  | 75W, 5VOUT Off-Line Power Transformer, ETD-29 |
| 1 | T2 | PE-68386 | Pulse Ing. | 1:1 Gate Drive Transformer |
| 1 | U1 | UCC2894PW | TI | Active Clamp, Current Mode PWM Controller |
| 1 | U2 | TL431ID | TI | Progr. Reference 2.5V,SO-8, Ind. |
|  | U3 | PC817 | Sharp | $5,3 \mathrm{kV}$ Through Hole Optocoupler |
|  | Z1 | FNR-10K471 |  | Varistor 470V, 45J |

